ENVE 301 Environmental Engineering Unit Operations

CHAPTER: 4

Gas transfer

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Removal of constituents

Chemical and/or biological conversion reactions

Transfer of material from one homogenous phase to another

Mass transfer

Principal applicationss of mass transfer operations in env. eng.:

Addition of gases to water (Absorption) (gas ---> liquid)

Removal of organics w/activated carbon (Adsorption) (liquid ---> solid) (gas ---> solid)

Removal of gases (gas stripping, desorption) (liquid \longrightarrow gas) (e.g., CO₂, O₂, H₂S, NH₃, VOC)

GAS TRANSFER



Gas transfer \longrightarrow process by which gas is transferred from one phase to another.

from gas phase \longrightarrow to liquid phase (Absorption)

from liquid phase _____ to gas phase (Desorption)

Applications in environmental engineering :

- \rightarrow Oxygen supply in aerobic process
- \rightarrow Transfer of chlorine (in the gas form) into the liquid for disinfection purposes.
- \rightarrow Transfer of ozone into the water.

 \rightarrow Removal of gases dissolved in water (H₂S, CH₄, NH₃)



If the liquid is initially pure with respect to the gas;

→ Gas molecules will migrate across the gas-liquid interface and become dissolved in the liquid (ABSORPTION)

Although some molecules of gas will begin leaving the liquid and returning the gas phase, the net reaction will be toward the liquid until a state of equilibrium is reached.

@ equilibrium:

the number of molecules leaving the liquid = the number of molecules entering the liquid again Liquid is said to be SATURATED. Important characteristic of this process:

- 1. SOLUBILITY of gas in water
- 1. TRANSFER RATE (rate at which absorption or desorption occur)

Solubility of Gas

The solubility of a gas in equilibrium with a liquid is quantified by **HENRY's LAW**

Solubility of a gas at constant temp. $\alpha\,$ Partial pressure of gas in contact with liquid

Dalton's law of partial pressure:

When a container is filled with a mixture of N gases, each gas exerts the some pressure as it would if it were the only gas in the vessel. The pressure of each component of the gas mixture (partial pressure) will depend solely on the number of moles of that gas present.

$$P_{total} = P_1 + P_2 + P_3 + \dots + P_N$$

$$\therefore \frac{\text{Partial pressure of a gas}(P_1)}{\text{Total pressure }(P_T)} = \frac{n_1}{n_1 + n_2 + \dots n_N}$$
Mole fraction of gas



Henry's constant \longrightarrow the unit of this parameter is variable (atm⁻¹; atm/mole fraction; , mg/l/atm ...)

highly variable with temperature

EXAMPLE 1:

Calculate the solubility of CO_2 (in air) in water at 25^oC and 1atm pressure. (CO_2 in air =0,03% H=6.11.10⁻⁴ atm⁻¹)

EXAMPLE 2:

Calculate the solubility of nitrogen (in air) in water at 0^oC and 1 atm pressure. (N₂ in air =79% H= $5.29.10^4 \frac{\text{atm}}{\text{mole fraction}}$)

EXAMPLE 3:

Calculate the solubility of O_2 (in air) in water at 20^oC , 1atm pressure. (O_2 in air 21% H=43,3mg/L/atm)

GAS TRANSFER RATE

The rate at which a gas transfer into solution can be described by Fick's first law;



 $\frac{dc}{dt} = K L_a (C_s - C)$

Value of $(C_s-C) \longrightarrow$ represents a concentration gradient.

As C approaches to Cs \longrightarrow transfer rate decreases.



depends on water quality type of aerator equipment

unique for each situation.

numerical values of K_{La} are usually determined experimentally.

$$\frac{dc}{dt} = K_{La} (C_s - C)$$

$$\begin{cases} \int \frac{1}{ax+b} dx = \frac{1}{a} Ln |ax+b| \\ \int C_0 \frac{dc}{C_s - C} = K_{La} \int \frac{1}{b} dt \\ 0 \end{cases}$$

$$- \ln (C_{s} - C)|_{C_{0}}^{C} = K_{La} t$$
$$- \ln (C_{s} - C_{t}) + \ln (C_{s} - C_{0}) = K_{La} t$$

$$\operatorname{Ln}(\operatorname{C}_{\mathrm{S}}-\operatorname{C}_{\mathrm{t}})-\operatorname{Ln}(\operatorname{C}_{\mathrm{S}}-\operatorname{C}_{\mathrm{0}})=-\operatorname{K}_{\operatorname{La}}\operatorname{t}$$

$$\operatorname{Ln} \frac{C_{\rm s} - C_{\rm t}}{C_{\rm s} - C_{\rm 0}} = -K_{\rm La}.t$$

$$A_s$$

$$\frac{C_s - C_t}{C_s - C_0} = e^{-K} La^{.t}$$

ABSORPTION OF GAS INTO A SOLUTION (It only takes place when C<Cs)

EXAMPLE 4 :

Dechlorinated secondary effluent is placed in a storage basin until needed for reuse. If the initial DO conc. is 1,5mg/L estimate the time required for the DO conc. to increase to 8,5mg/L due to surface re-aeration assuming the water in storage basin is circulated and not stagnant. Assume the K_L value for oxygen is equal to 0,03m/h. The surface area of the storage basin is 400m² and the depth is 0,025m.T=20°C

DESORPTION OF GAS INTO A SOLUTION

h



DESORPTION OF GAS FROM A SOLUTION (If the conc. of specific volatile chemical is not common to atmosphere $C_s \cong 0$

As

 $\forall = A_s.h$

EXAMPLE:

A quantity of benzene was spilled accidently into a treated wastewater storage basin having depth of 2m. Estimate the time required for the concentration of benzene to drop out 50% from the initial concentration due to volatilization. K_{I} for benzene = 0,144 m/hr

TWO FILM THEORY (Lewis – Whitman)

The resistance to movement between the phases can be explained by <u>TWO-FILM THEORY</u> (Lewis-Whitman)

Acc. to this theory, transfer of a gas must occur across the two films that are assumed to exist at the gas-liquid interface.



Figure 3-2 Two-film model of the interface between gas and liquid: (*a*) absorption mode and (*b*) desorption mode.

(e.g. Ammonia)

Gases that are highly soluble in water \longrightarrow Encounter more resistance in passing through the gas film. GAS-FILM CONTROLLED.

Gases that are slightly soluble in water \longrightarrow Encounter more resistance in passing through liquid film. (e.g. Oxygen, Nitrogen) LIQUID-FILM CONTROLLED.

Gases of intermediate solubility

----> Encounter approximately equal resistance through the films. (MIXED FILM CONTROLLED)