

ENVE 301

Environmental Engineering Unit Operations

Lecture 7

Mixing

SPRING 2014

Assist. Prof. A. Evren Tugtas



Mixing

- Mixing liquids is used to:
 - Blending of two immiscible liquids (ethyl alcohol/water)
 - Dissolving solids in liquids
 - Dispersing a gas in a liquid as fine bubbles
 - Agitation of the fluid to increase heat transfer
- Mixing in water treatment is used to:
 - achieve coagulation
 - achieve flocculation

Mixing Chemicals in Water Treatment

- Coagulation
 - Coagulants
- Disinfection
 - Chlorine contact chamber (Chlorine is mixed with water)
 - Ozone contact chamber (Ozone is mixed with water)

Mixing

- Mixing can occur in following locations;
 - Water intake (Pumps, pipes)
 - Flash mix tanks
 - Flocculation tanks
 - Other

Mixing

- Three phenomena contribute to mixing;

1) Molecular diffusion

Diffusion: Random motion of molecules from high concentration to low concentration

Molecular Diffusion: Moving molecules self propelled by thermal energy, not affected by concentration (Brownian motion)

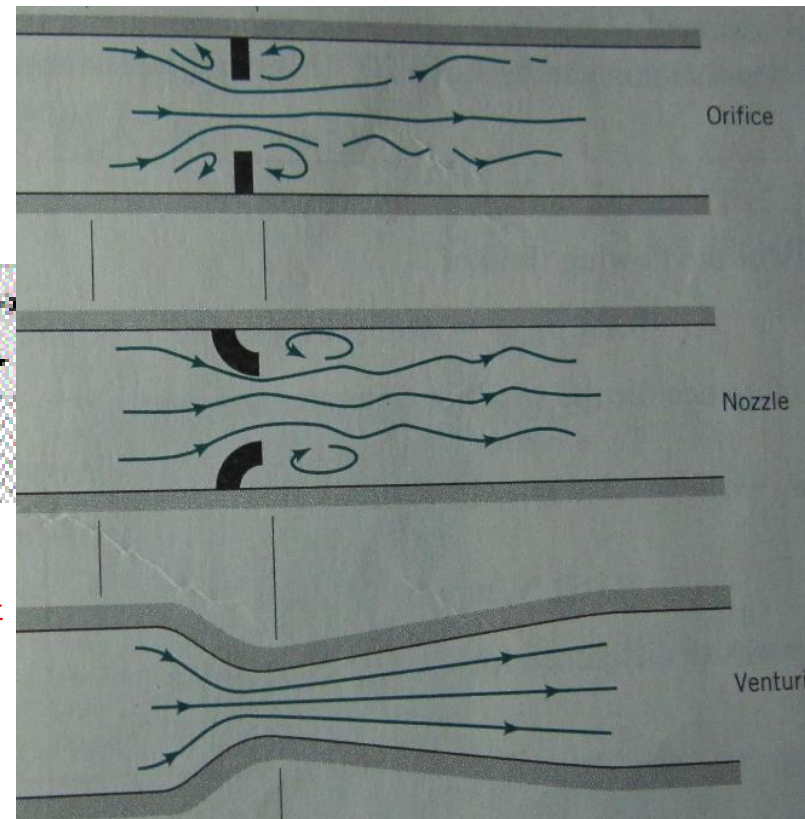
Ref:

Marr <http://webworld.unesco.org/water/ihp/db/glossary/glu/EN/GF0330EN.HTM>
University



Mixing

- Three phenomena contribute to mixing;
- 2) Eddy Current (Circular flow): Water flows opposite to the original flow (whirlpools – function of a degree of turbulence)



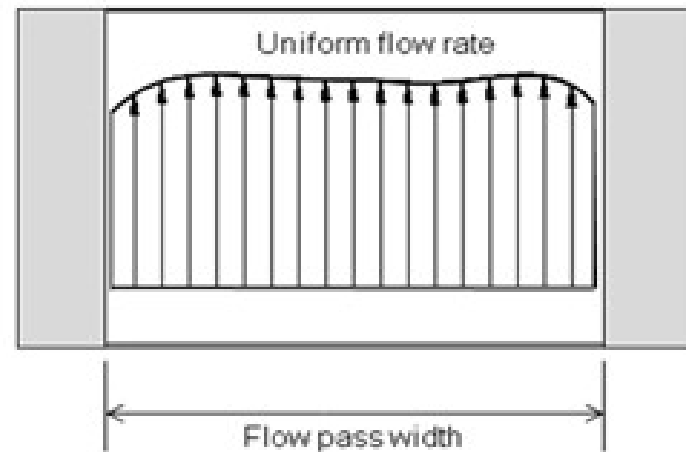
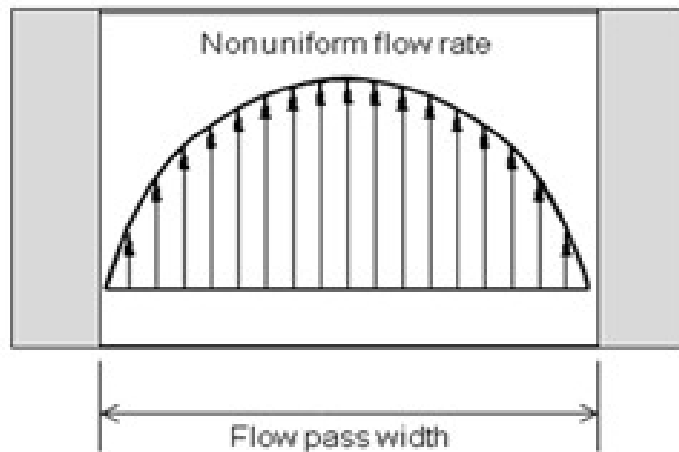
Ref:

http://ohiodnr.com/water/pubs/fs_st/stfs20/tabid/4175/Default.aspx

Munson BR, Young DF, Okiishi TH. Fundamentals of Fluid Mechanics. 1998. ISBN: 0-471-17024-0

Mixing

3) Non-uniform flow: At any given time, velocity is not same at every point of the flow.



Ref: <http://en.engormix.com/MA-aquaculture/articles/aquafeed-extrusion-t1669/p0.htm>

Factors that affect mixing

- Number of particles
- Size of particles
- Mixing time
- Water temperature
- Chemical dosage

Mixing

- Power input per unit volume of liquid can be used as a rough measure of mixing effectiveness.
- More input power creates more turbulence, and greater turbulence leads to better mixing
- Power imparted to the water can also be measured by the **Velocity Gradient** (Camp, 1955)

Velocity Gradient (G) for mechanical or pneumatic mixing

$$G = \sqrt{\frac{P}{\mu V}}$$

Velocity gradient → Ratio of relative velocity of two particles to the distance between the particles

- Rate of particulate collision is proportional to G
- G must be sufficient enough to achieve desired rate of collisions

P: Power imparted to the water (Nm/s OR W)

μ : Absolute viscosity of water (Ns/m²)

V: Basin volume (m³)

G: Velocity gradient (s⁻¹)

Example -1

- Two particles moving 1.5 m/sec relative to each other at a distance of 0.05 m would have a velocity gradient of :

$$G = \frac{1.5 \text{ m/s}}{0.05 \text{ m}} = 30 \text{ s}^{-1}$$

Velocity Gradient (G) for baffle basin

$$G = \sqrt{\frac{\gamma h_L}{\mu T}}$$

γ : specific weight of water (kgm^2/s^2 OR kN/m^3)

μ : Absolute viscosity of water (Ns/m^2)

h_L : head loss (m)

T: detention time (s)

G: Velocity gradient (s^{-1})

Mixers

1) Hydraulic mixing devices

- a) Venturi sections, Orifices
- b) Hydraulic jumps
- c) Parshall flume
- d) Weirs
- e) Baffled mixing devices
- f) Static mixers

2) Mechanical mixing devices

- a) Propeller mixer
- b) Turbine mixer
- c) Paddle mixer

3) Pneumatic mixers

- a) Air diffusers

Hydraulic Mixers

- Principally identified by their lack of moving parts.
- In-line mixers are commonly used for the mixing of chemicals
- Over and under baffle channels are used for flocculation
- Degree of turbulence is measured by the loss in head

Power dissipation in a hydraulic mixer;

$$P = \gamma Q h_L = \rho g Q \Delta h_L$$

γ =specific weight of water (kgm^2/s^2 OR kN/m^3)

ρ =density of water (kg/m^3)

g =gravitational acceleration (m/s^2)

Q =flow rate (m^3/s)

h_L =headloss (m)

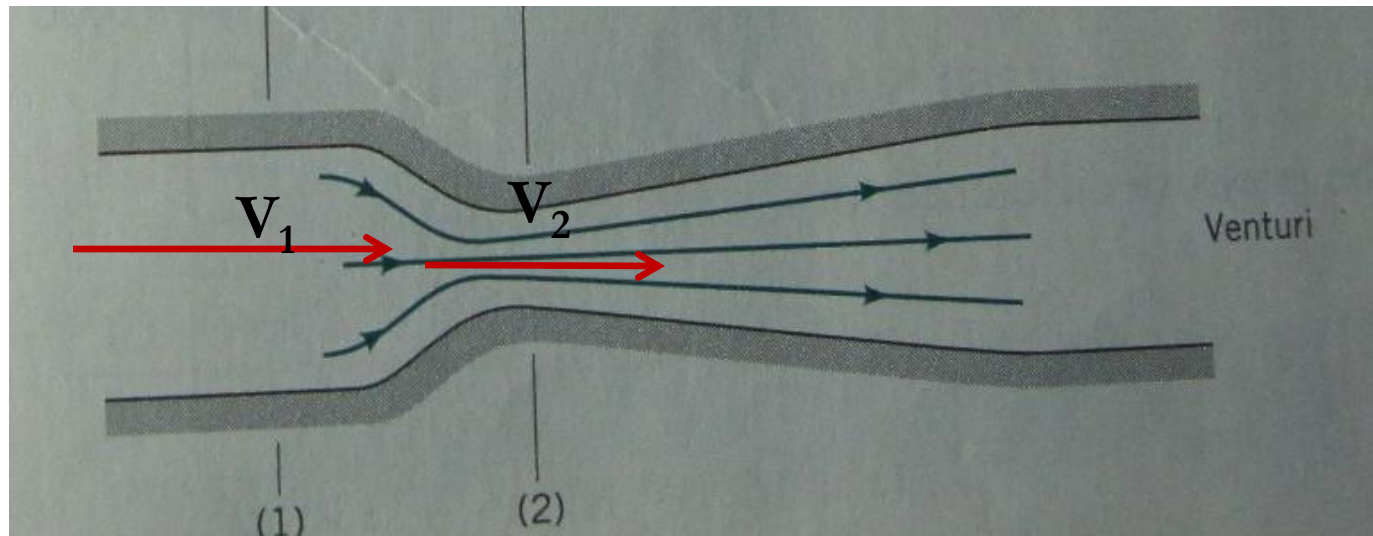
Hydraulic Mixers

Venturi Sections

- Turbulance is generated at the throat, which causes mixing

$$h_L = C_D \frac{V_2^2}{2g}$$

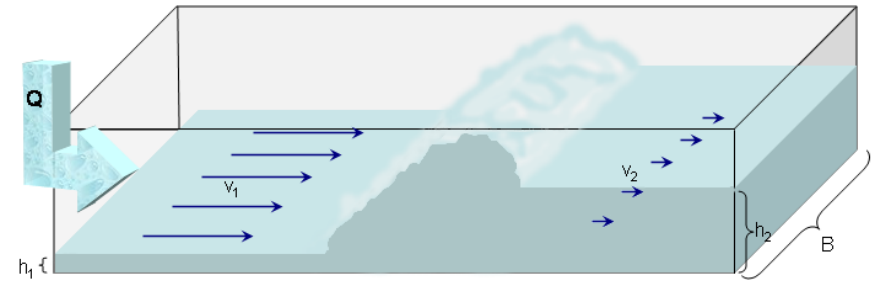
C_D : coefficient of discharge



Ref: Munson BR, Young DF, Okiishi TH. Fundamentals of Fluid Mechanics. 1998. ISBN: 0-471-17024-0

Hydraulic Mixers

Hydraulic Jumps



Q : flow rate
 B : channel width
 h_1 : upstream depth
 v_1 : upstream velocity
 h_2 : downstream depth
 v_2 : downstream velocity

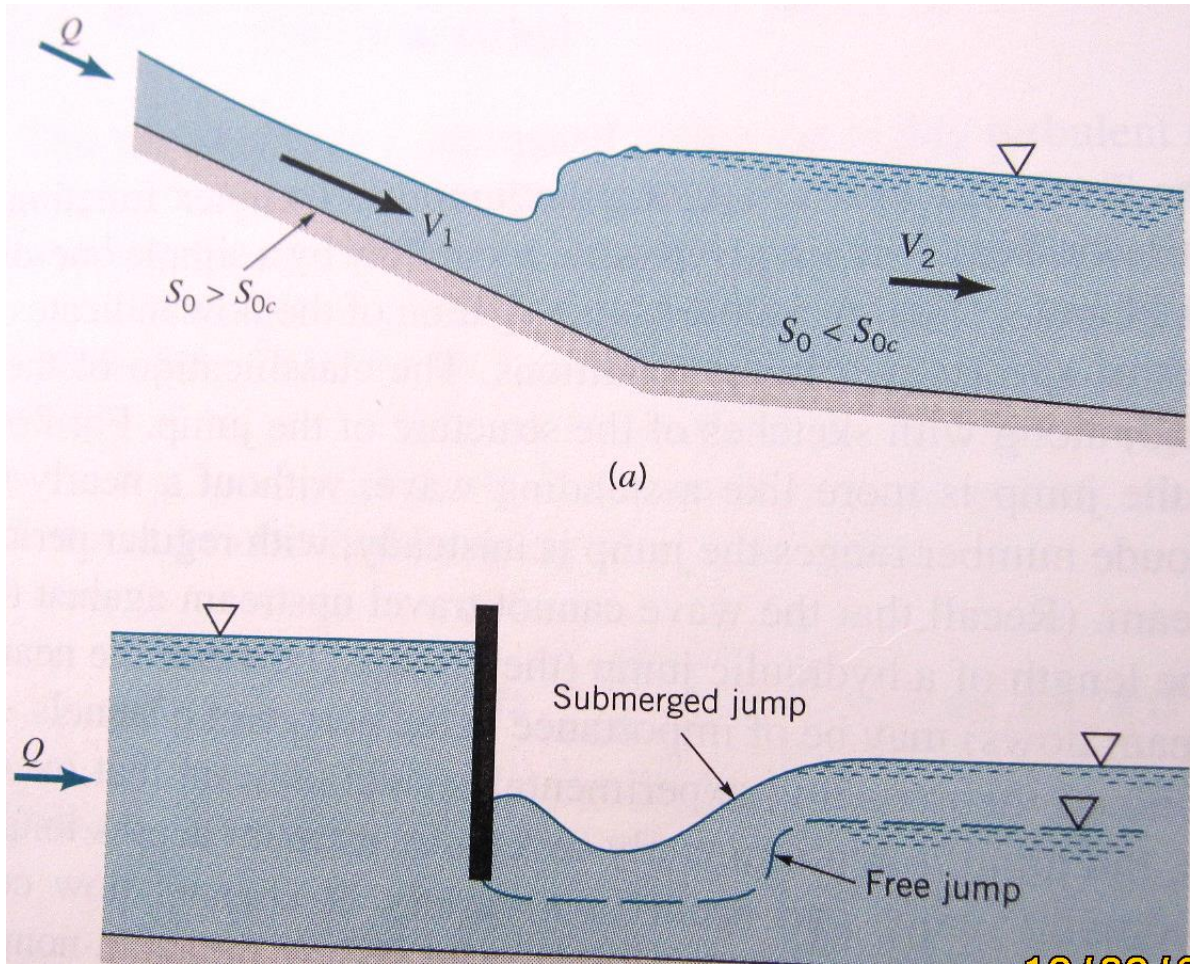
Ref: <http://www.philip-lutzak.com/weather/GRAVITY WAVES - GOM/GRAVITY WAVES - GOM HOME.htm>

Ref:
<http://einstein.atmos.colostate.edu/~m-cnoldy/HydraulicJump.html>

- Water flow creates supercritical flow
- Turbulence generated in the jump, which causes effective mixing

Hydraulic Mixers

Hydraulic Jumps



- Jump caused by a change in channel slope

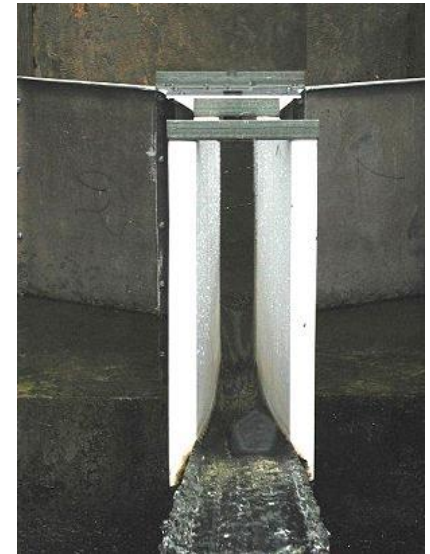
- Submerged jump

Ref: Munson BR, Young DF, Okiishi TH. Fundamentals of Fluid Mechanics. 1998. ISBN: 0-471-17024-0

Hydraulic Mixers

Parshall Flume

- Parshall flumes are devices used to measure flow of water in open channels. They are modified versions of venturi meters.
- The flume consists of a converging section with a level floor, a throat section with a downward sloping floor, and a diverging section with an upward sloping floor.
- Effective mixing occurs when hydraulic jump is followed by downstream of a flume
- On the basis of throat width partial flumes can be:
 - Very small - 25.4 mm to 76.2 mm.
 - (Small 152.40 mm to 2438.4 mm.
 - Large 3048 mm to 15240 mm.



Ref:http://www.flowmeterdirectory.com/pa_rshall.html

Hydraulic Mixers

Parshall Flume

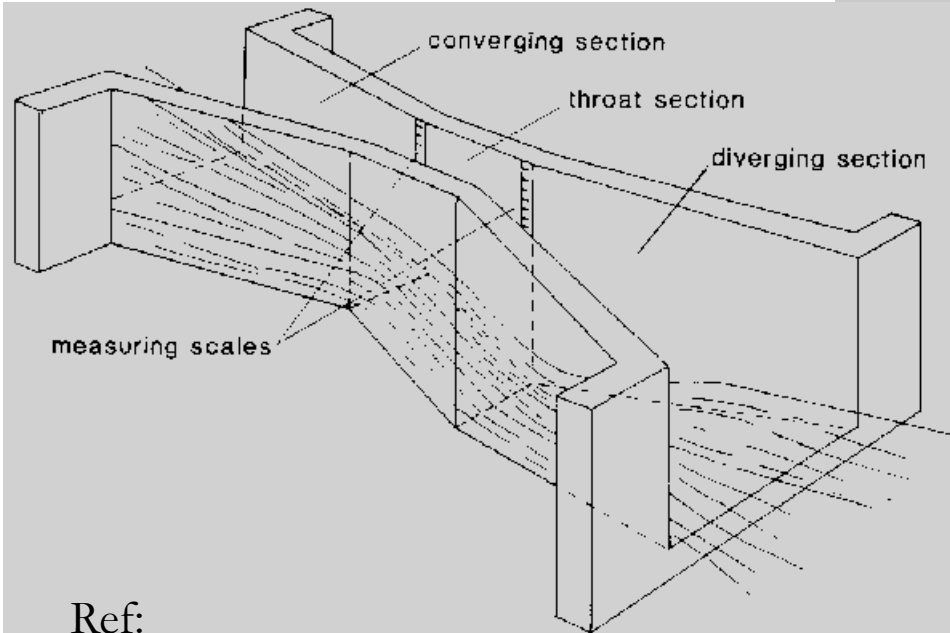
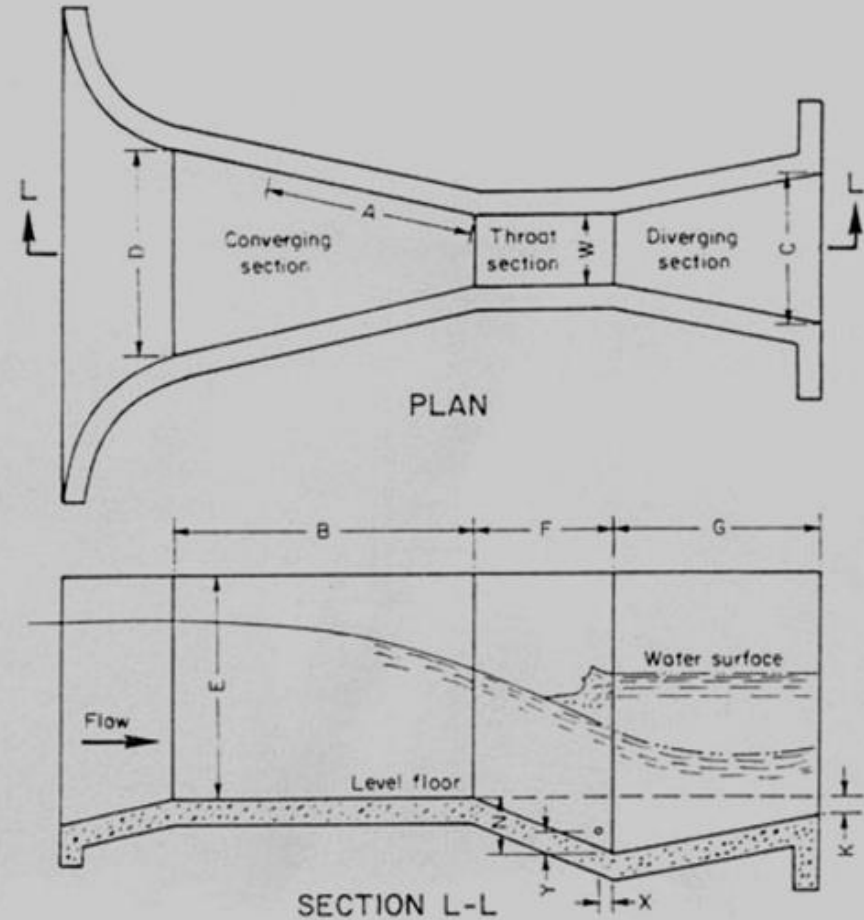


FIGURE 33
Dimensions of a Parshall flume (USDA-SCS 1965)



Ref:

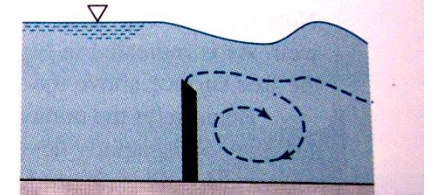
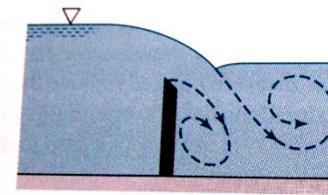
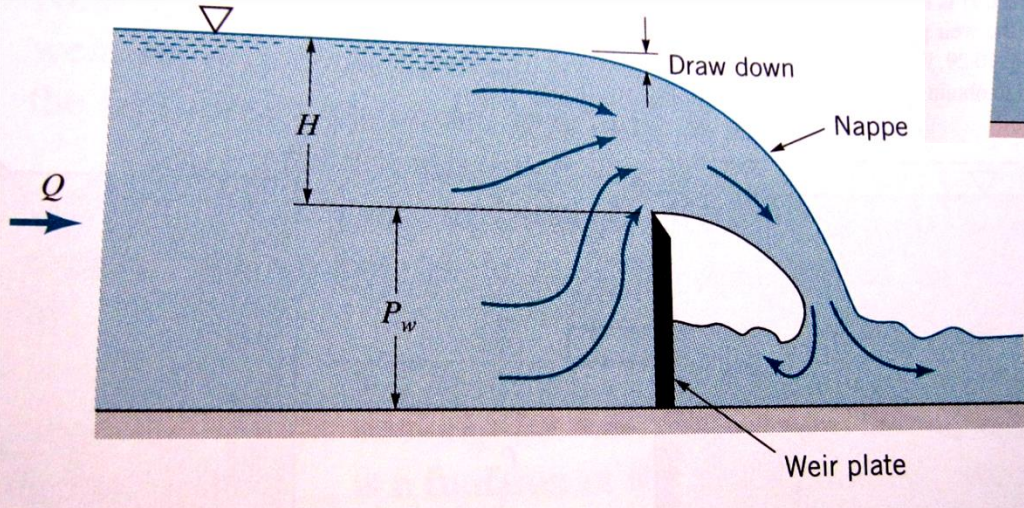
<http://www.fao.org/docrep/R4082E/r4082e06.htm>

Ref: <http://www.fao.org/docrep/T0848E/t0848e-09.htm>

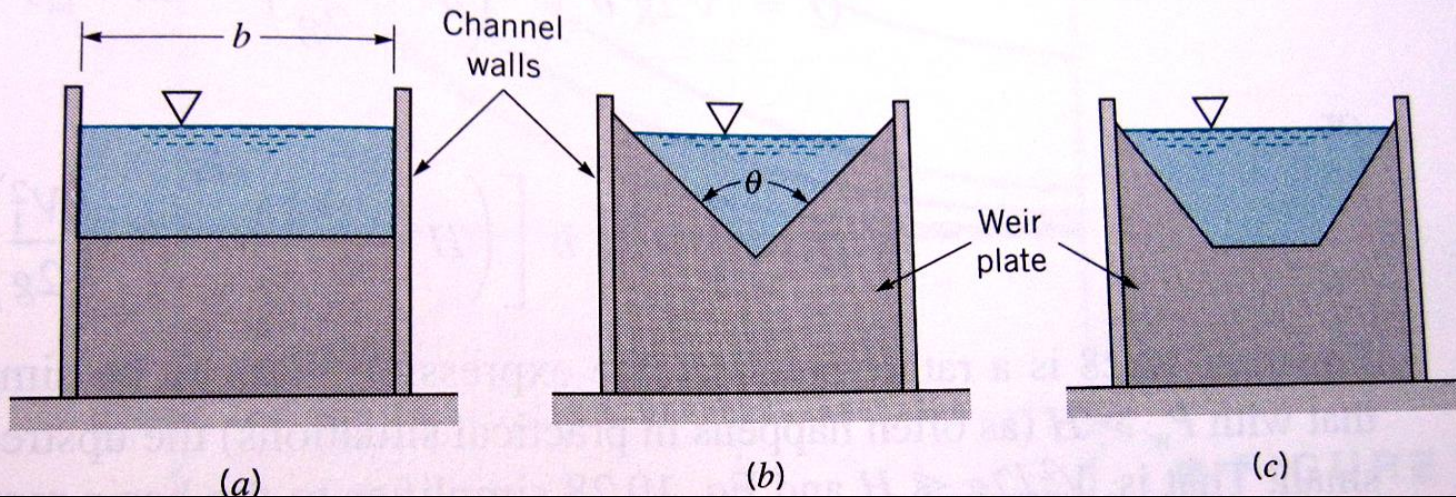
Hydraulic Mixers

Weirs

- A weir is an obstruction on a channel bottom over which the fluid must flow.



Ref: Munson BR, Young DF, Okiishi TH. Fundamentals of Fluid Mechanics. 1998. ISBN: 0-471-17024-0



Hydraulic Mixers

Weirs

- A sudden drop in a hydraulic level over a weir induces the turbulence in water → causes mixing
- Vertical fall over the weir should be at least **0.1 m** to ensure sufficient mixing
- The height of the coagulant diffused over the weir should be at least **0.3 m** to penetrate the nappe thickness.

Hydraulic Mixers

Weirs



Both pictures are the courtesy of
Assist. Prof. Bilge Alpaslan Kocamemi



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Hydraulic Mixers

Baffled Mixing Chambers

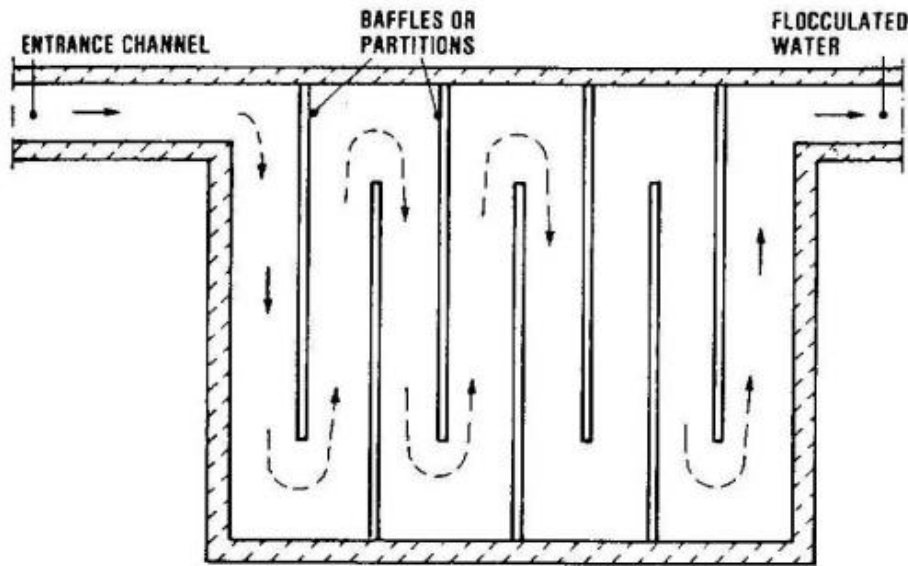


Figure 6.2. Horizontal-flow baffled channel flocculator (plan). Source: IRC, 1981b.

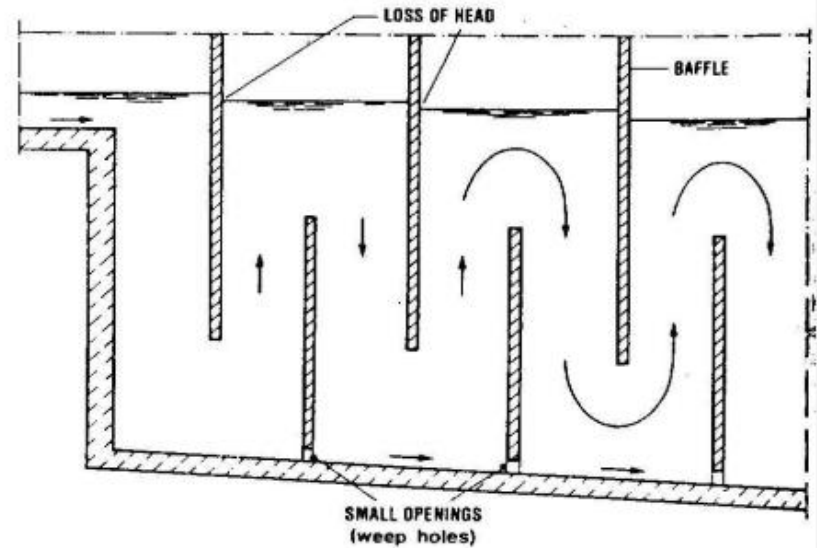


Figure 6.3. Vertical-flow baffled channel flocculator (cross-section). Source: IRC, 1981b.

Ref: Schulz & Okun, 1984, John Wiley & Sons

- Mixing achieved by reversing the flow through the openings

- Around the end: Horizontal-flow baffles
- Over and Under: Vertical-flow baffles

- Baffles mainly used for flocculation

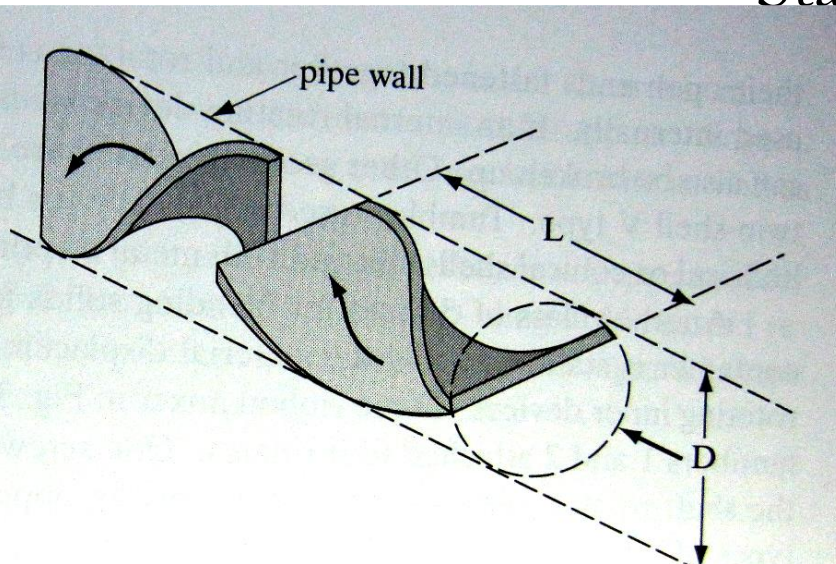
Hydraulic Mixers

Static Mixers

- Static mixers are principally identified by their lack of moving parts.
- Static mixers contain elements that bring about sudden changes in the velocity patterns as well as momentum reversals
- Mixing occurs in a plug flow regime: the longer the mixer, the better the mixing → higher headloss
- Mixing time is quite short; typically less than 1 sec.
- In-line mixers are commonly used for the mixign of chemicals

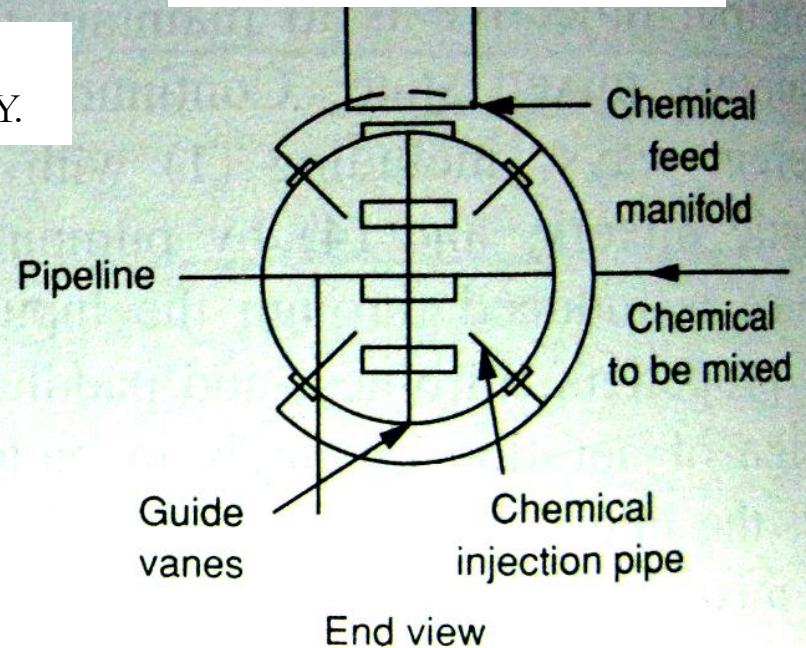
Hydraulic Mixers

Static Mixers

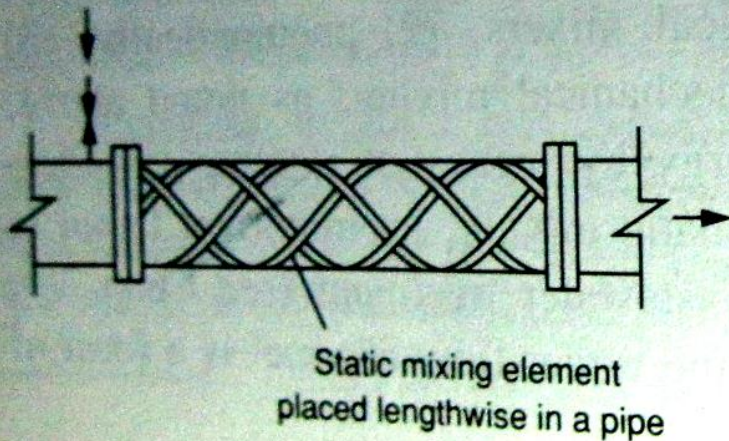


Ref: Munson BR, Young DF, Okiishi TH. Fundamentals of Fluid Mechanics. 1998. ISBN: 0-471-17024-0

In-line turbine mixer



•Metcalf & Eddy, Inc. (2003). *Wastewater Engineering-Treatment and Reuse*, 4th ed., McGraw-Hill, New York, NY.



(d)

Mechanical Mixers

Turbine or Propeller Mixers

- Mechanical mixing is reliable, very effective and flexible in operation
- Mechanical mixing basins are not affected to any extent by variation in the flowrate.
- Mechanical mixing basins have low head losses.

Mechanical Mixers

Turbine or Propeller Mixers *Vortexing*

- Vortexing may occur: Liquid to be mixed may rotate with the impeller
- Vortexing causes the difference between the impeller velocity and water velocity to decrease, which decreases effectiveness of mixing



Ref:

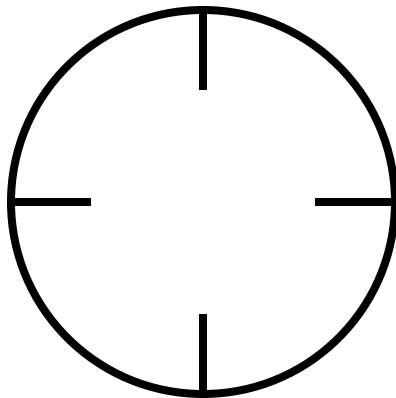
<http://www.flickr.com/photos/esaruoho/favorites/?view=lg>

Mechanical Mixers

Turbine or Propeller Mixers *Vortexing*

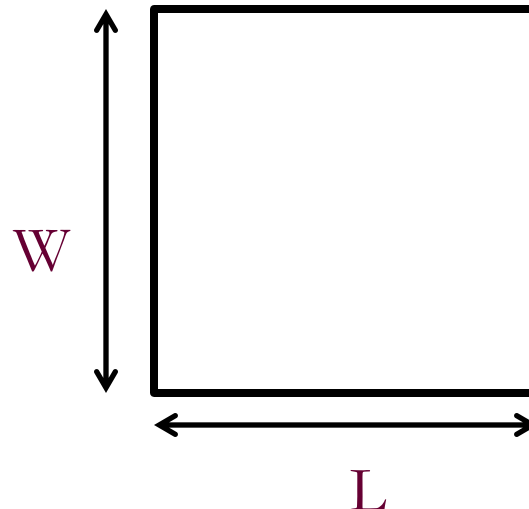
To eliminate vortexing:

- Four baffles can be placed vertically at the tank wall. Each baffle width = 10% - 12% of the tank diameter



$$\text{Baffle width} = 1/10D$$

$$\text{Baffle width} = 1/10\sqrt{WL}$$



Mechanical Mixers

Turbine or Propeller Mixers *Vortexing*

- To prevent vortexing in small tanks
 - Impeller should be mounted off-center
 - Impeller can be mounted at an angle
 - Impeller can be mounted to the side of basins at angle

Turbine or propeller mixers are usually constructed with a vertical shaft driven by a speed reducer and electric motor

Types of impellers:

1. Radial flow impellers

Generally have flat or curved blades located parallel to the axis of shaft

2. Axial flow impellers

3. Make an angle of less than 90° with drive shaft

Mechanical Mixers

Turbine or Propeller Mixers *Power Requirement*

- Laminar Flow;
- $Re < 10$ to 20

$$P = K_L \mu n^2 D_i^3$$

Power imparted by baffled or unbaffled tank

- Turbulent Flow;
- $Re > 10000$

$$P = K_T \rho n^3 D_i^5$$

Power imparted by baffled tank

P=Power requirement (Nm/s)

K_L =Impeller constant for laminar flow

K_T =Impeller constant for turbulent flow

n=rotational speed (rps)

D_i =Impeller diameter (m)

ρ =density of the liquid (kg/m^3)

γ =Specific weight of the liquid (N/m^3)

μ =dynamic viscosity (Ns/m^2)

$$Re = \frac{D_i^2 n \rho}{\mu}$$

Mechanical Mixers

Turbine or Propeller Mixers *Power Requirement*

In laminar flow → power imparted is independent of the presence of baffles

In turbulent flow →

Power imparted in an unbaffled tank = 1/6 of the power imparted in the same tank with baffles

Power imparted in an unbaffled square tank = 75% of the power imparted in a baffled square or a baffled circular tank

Power in a baffled vertical square tank = Power in a baffled vertical circular tank having D =width of square tank

Mechanical Mixers

Turbine or Propeller Mixers *Power Requirement*

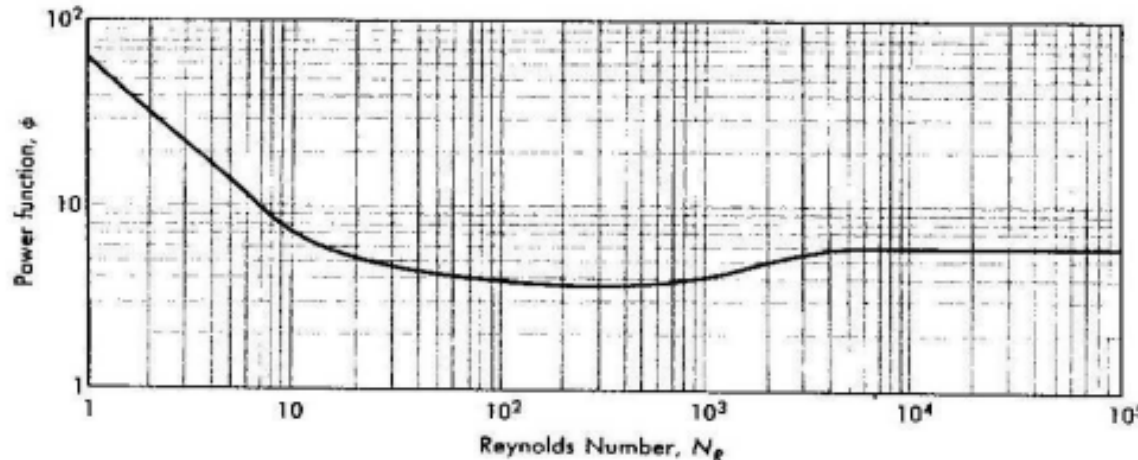
TABLE 8.2 Values of Constants K_L and K_T in Eqs. (8.11) and (8.12) for Baffled Tanks Having Four Baffles at Tank Wall, with Width Equal to 10% of the Tank Diameter

| TYPE OF IMPELLER | K_L | K_T |
|---|-------|-------|
| Propeller, pitch of 1, 3 blades | 41.0 | 0.32 |
| Propeller, pitch of 2, 3 blades | 43.5 | 1.00 |
| Turbine, 4 flat blades, vaned disc | 60.0 | 5.31 |
| Turbine, 6 flat blades, vaned disc | 65.0 | 5.75 |
| Turbine, 6 curved blades | 70.0 | 4.80 |
| Fan turbine, 6 blades at 45° | 70.0 | 1.65 |
| Shrouded turbine, 6 curved blades | 97.5 | 1.08 |
| Shrouded turbine, with stator, no baffles | 172.5 | 1.12 |
| Flat paddles, 2 blades (single paddle), $D_i/W_i = 4$ | 43.0 | 2.25 |
| Flat paddles, 2 blades, $D_i/W_i = 6$ | 36.5 | 1.70 |
| Flat paddles, 2 blades, $D_i/W_i = 8$ | 33.0 | 1.15 |
| Flat paddles, 4 blades, $D_i/W_i = 6$ | 49.0 | 2.75 |
| Flat paddles, 6 blades, $D_i/W_i = 6$ | 71.0 | 3.82 |

• Reynolds, T. D., and P. A. Richards. Unit Operations and Processes in Environmental Engineering. 2nd ed. Boston, MA: PWS Publishing Company, 1996.

Mechanical Mixers

Turbine or Propeller Mixers *Power Requirement*



Power imparted in an unbaffled tank (valid for laminar and turbulent flow)

FIGURE 12.9 Ref: Tchobanoglous and Schroeder, 1985, Addison-Wesley Publishing Company

Mixing power function curve for standard tank configuration shown in Fig. 12.8.
Source: Adapted from Ref. [12.23].

$$\phi = \text{Power function dimensionless} = \frac{P}{\rho N^3 D^5}$$

$$\phi = k R_e^P$$

k = constant of an impeller tank geometry

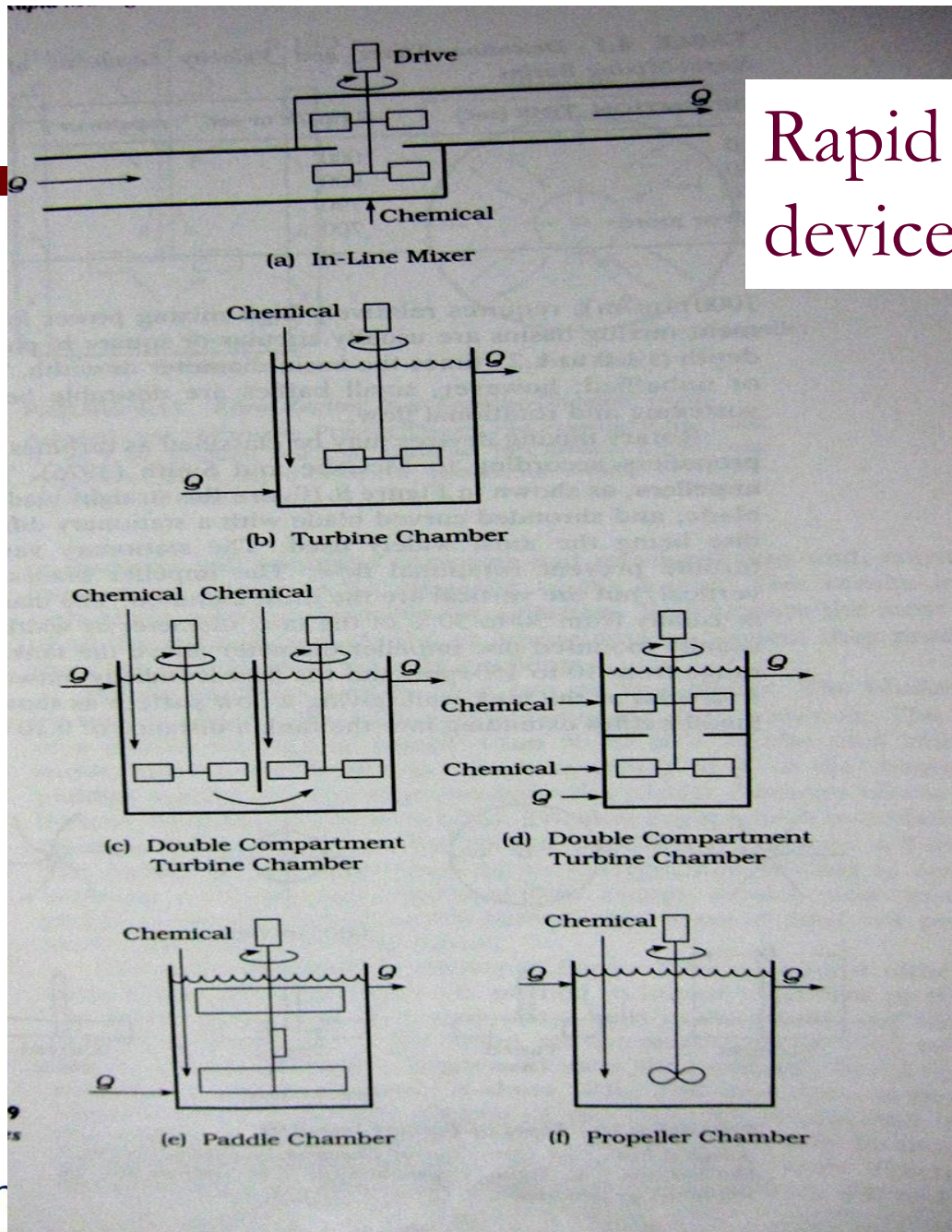
P = -1 (for laminar)

P = 0 (for turbulent)

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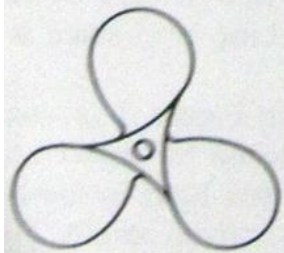
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Kocamemi

Rapid mixing devices



Ref: Reynolds, T. D., and P. A. Richards. Unit Operations and Processes in Environmental Engineering. 2nd ed. Boston, MA: PWS Publishing Company, 1996.

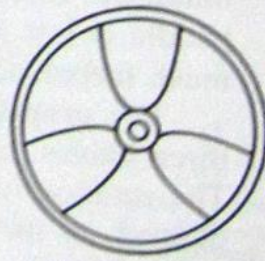
Propeller Impellers



(a) Standard Three Blade



(b) Weedless



(c) Guarded

Ref: Reynolds, T. D., and P. A. Richards. Unit Operations and Processes in Environmental Engineering. 2nd ed. Boston, MA: PWS Publishing Company, 1996.

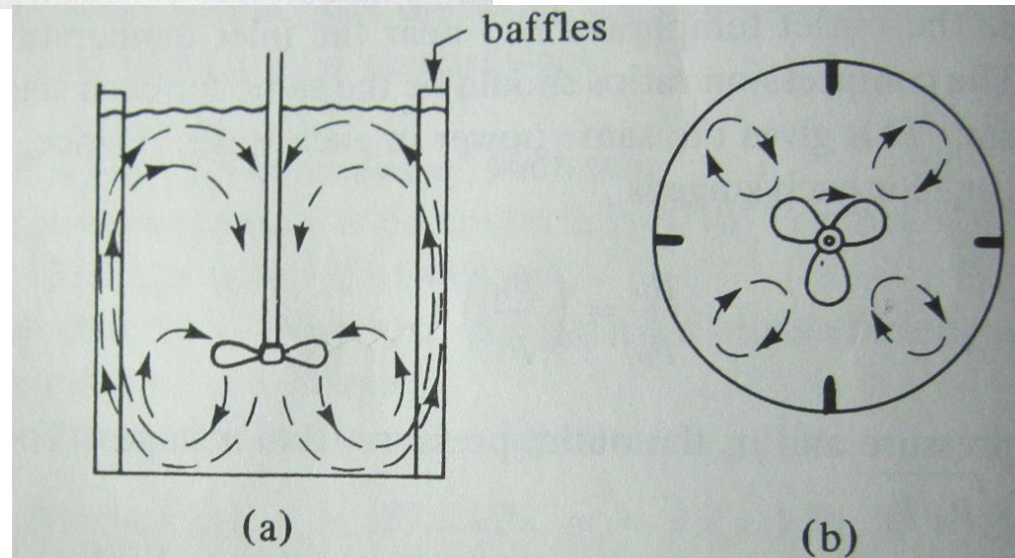


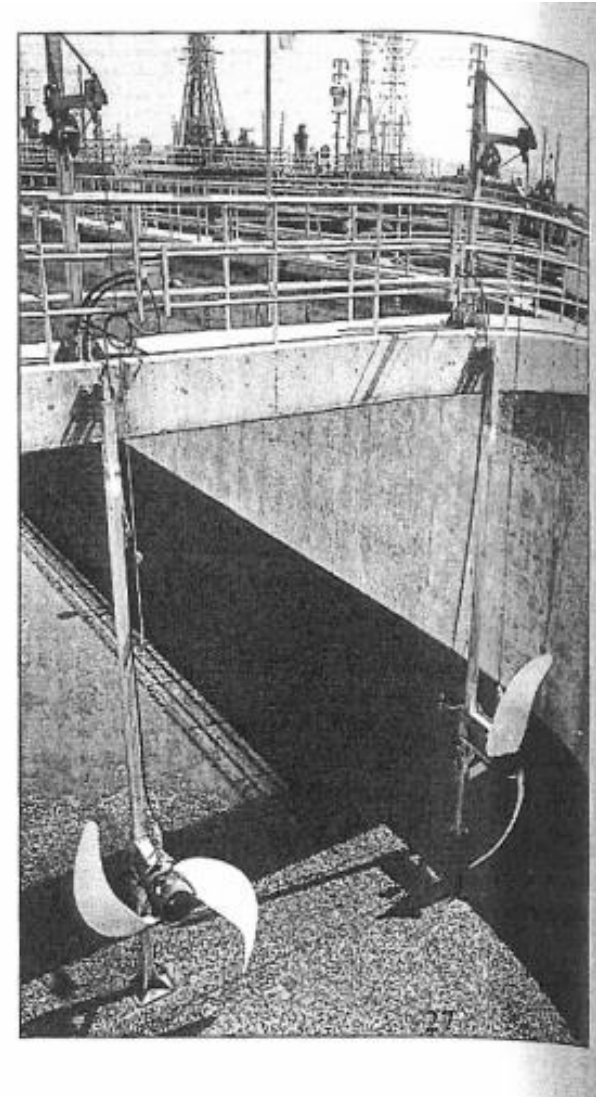
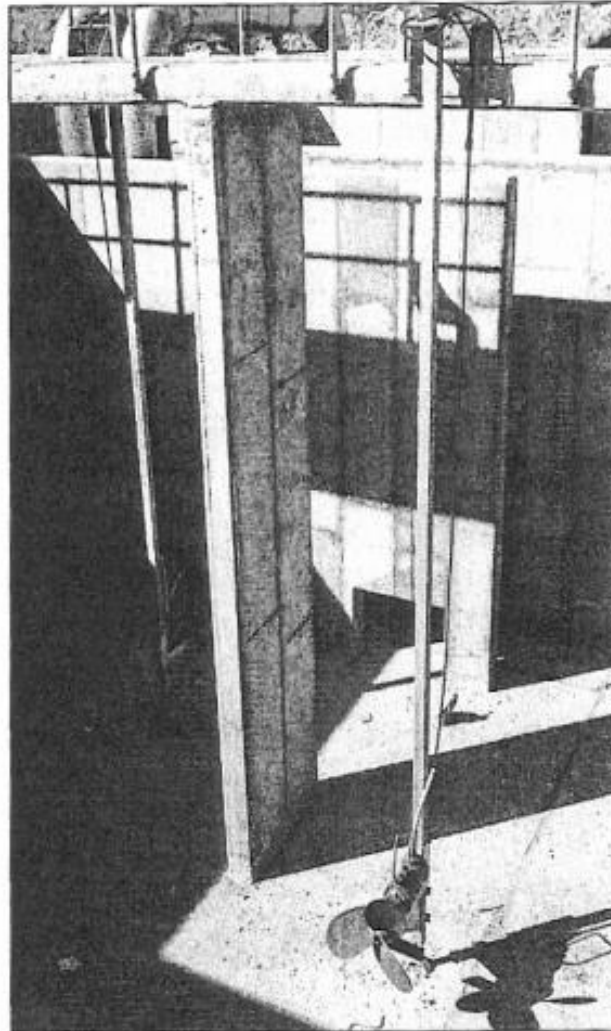
FIGURE 3.4-1. *Baffled tank and three-blade propeller agitator with axial-flow pattern: (a) side view, (b) bottom view.*

Propeller Mixer

Propeller Mixer

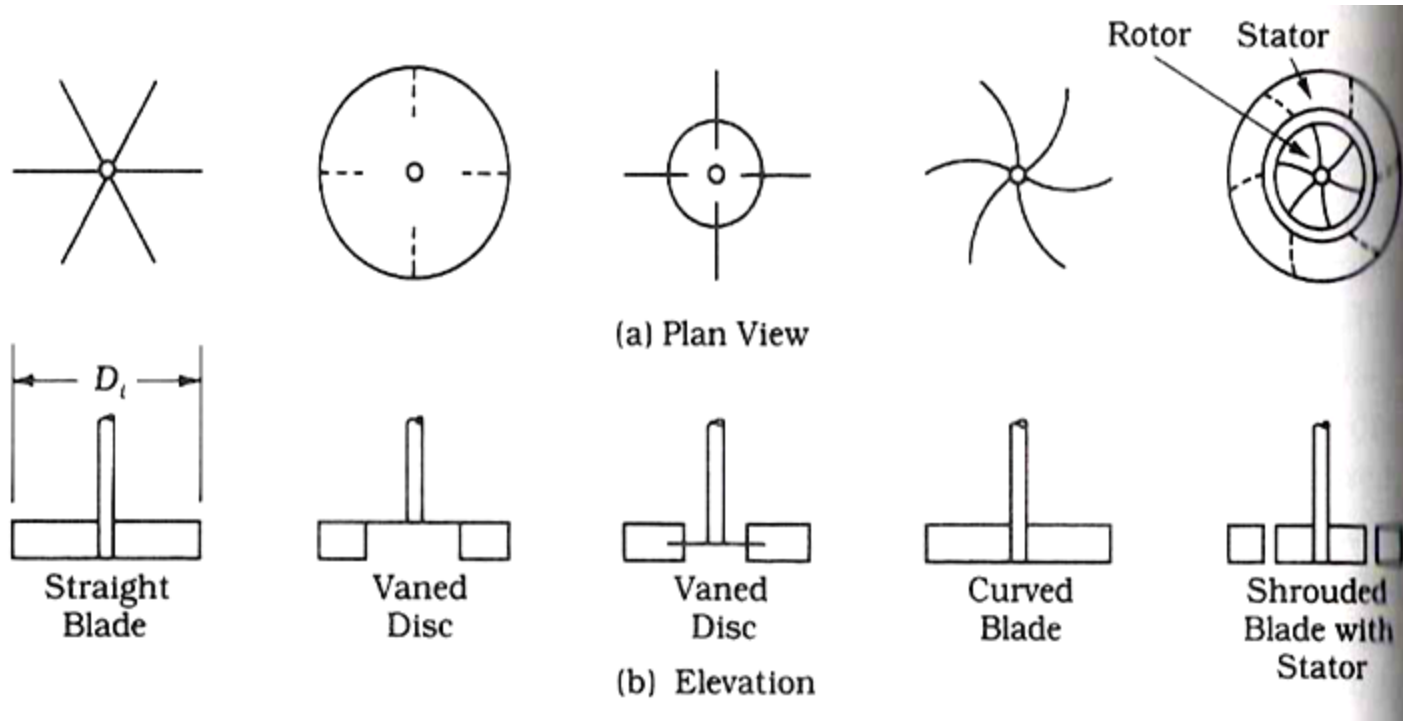
Submerged propeller mixers used to mix the contents of an anoxic reactor.

ref: Metcalf Eddy, 1991, McGraw Hill



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Turbine Impellers



Ref: Reynolds, T. D., and P. A. Richards. Unit Operations and Processes in Environmental Engineering. 2nd ed. Boston, MA: PWS Publishing Company, 1996.

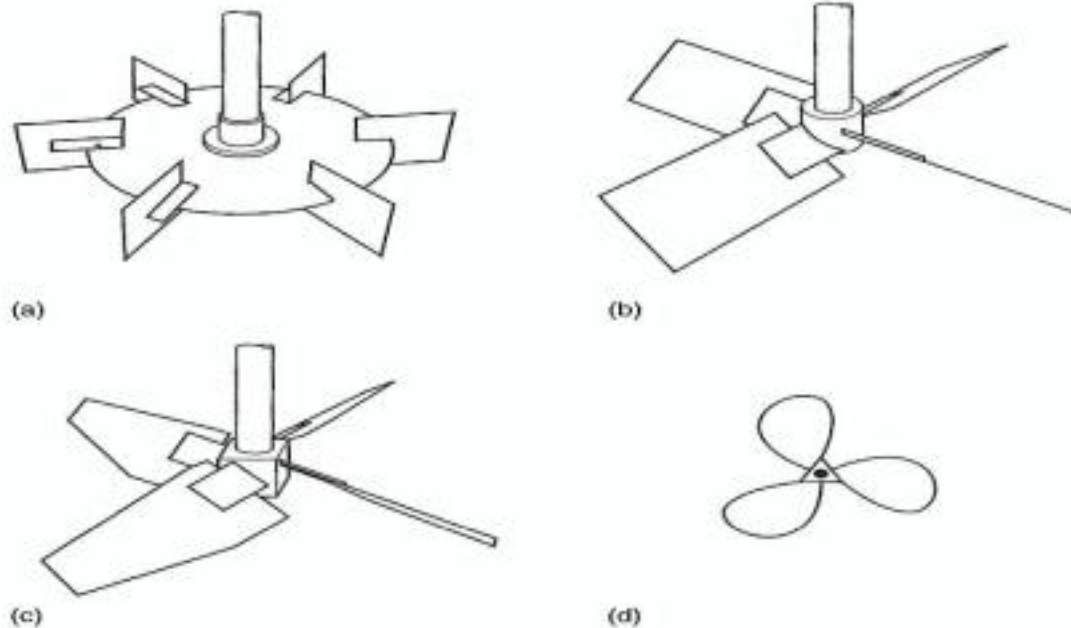
Turbine Impellers

Figure 5-15

Typical impellers used for mixing in wastewater-treatment facilities:

(a) disk-type radial-flow impeller, (b) axial-flow pitched (typically 45°) blade impeller, (c) axial-flow hydrofoil-type impeller, and (d) propeller mixer.

Note: The flat blade radial-flow turbine mixer looks like the axial-flow impeller (b) with the exception that the blades are set parallel to the axis of the shaft.



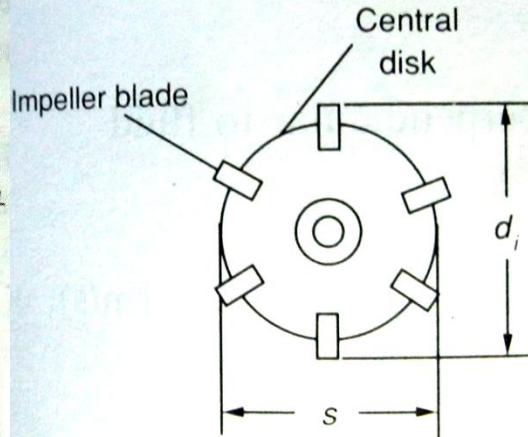
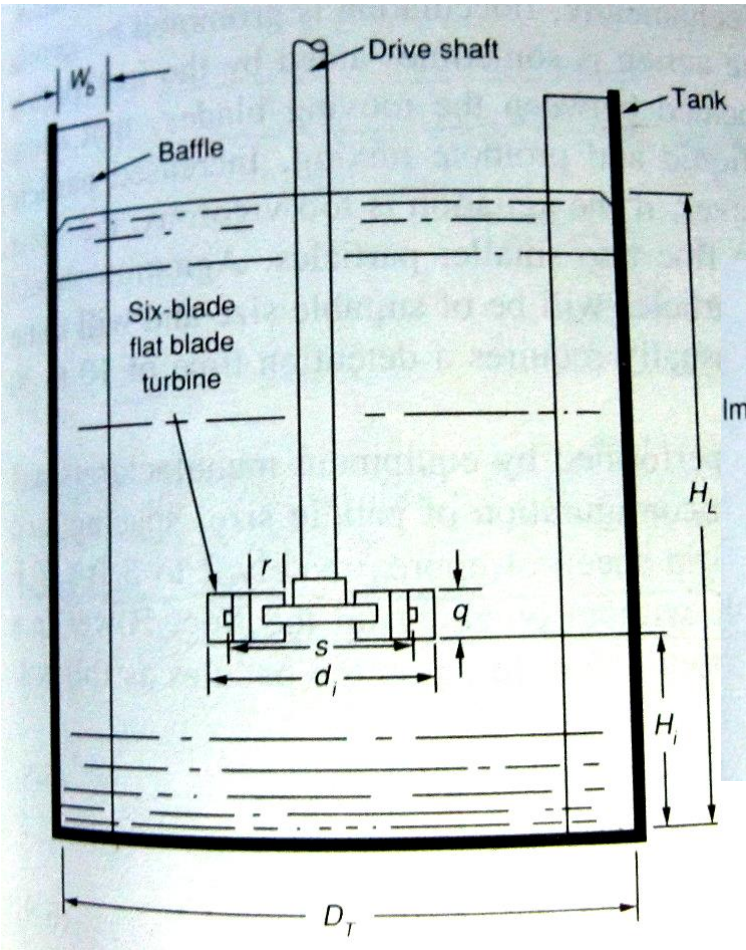
Ref: Metcalf Eddy, 1991, McGraw Hill

Table 5-11

Typical types of mixing impellers used in wastewater treatment^a Ref: Metcalf Eddy, 1991, McGraw Hill

| Type of impeller | Flow | Shear | Pumping capacity | Applications |
|---------------------------------------|--------|----------|------------------|--|
| Vertical flat blade turbine (VFBT) | Radial | High | Low | Vertical-flow flash mixing, suspension of solids, gas dispersion |
| Disk turbine | Radial | High | Low | Mixing, gas dispersion |
| Surface impeller | Radial | High | Moderate | Gas transfer |
| Pitched-blade turbine (45 or 32° PBT) | Axial | Moderate | Moderate | Horizontal flash mixing, suspension of solids |
| Low-shear hydrofoil (LS) | Axial | Low | High | Horizontal-flow flash mixing, suspension of solids, blending, flocculation |
| Propeller | Axial | Very low | High | Horizontal-flow flash mixing, suspension of solids, blending, flocculation |

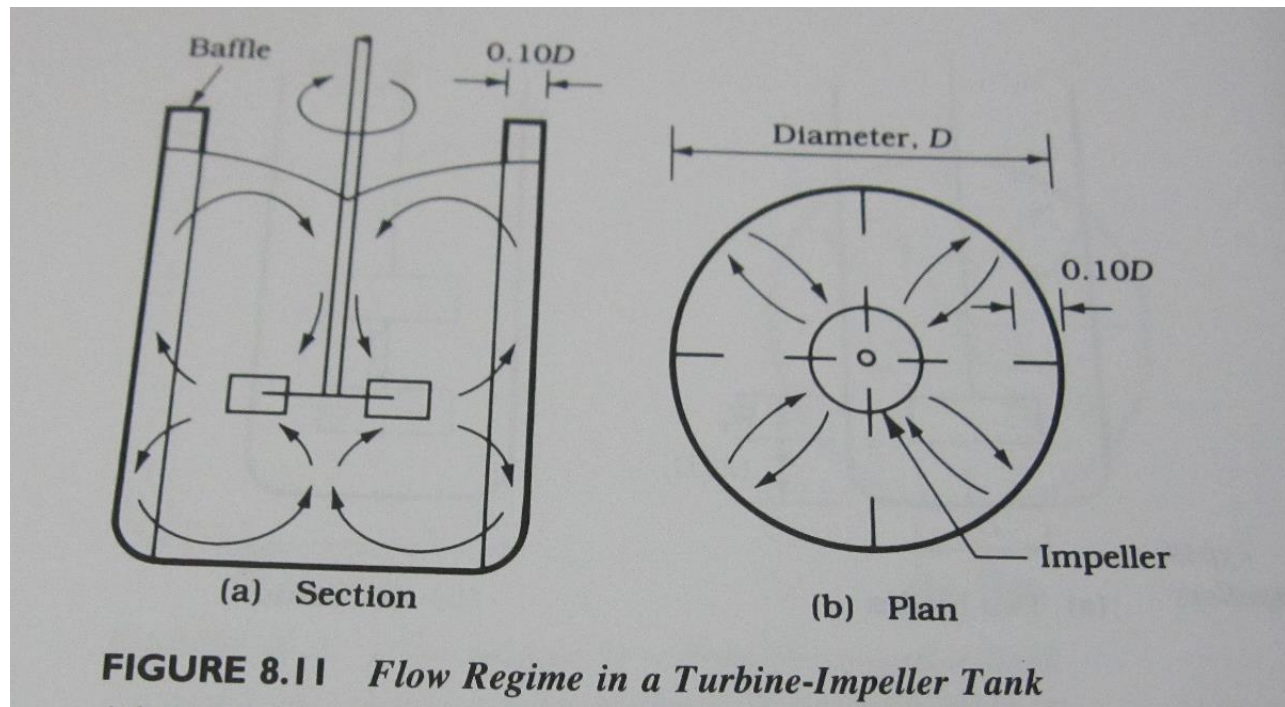
Turbine impeller in a baffled tank



- Notes:
1. The agitator is a six-blade flat turbine impeller
 2. Impeller diameter, $d_i = 1/3$ tank diameter
 3. Impeller height from bottom, $H_i = 1.0$ impeller diameter
 4. Impeller blade width, $q = 1/5$ impeller diameter
 5. Impeller blade length, $r = 1/4$ impeller diameter
 6. Length of impeller blade mounted on the central disk = $r/2 = 1/8$ impeller diameter
 7. Liquid height, $H_L = 1.0$ tank diameter
 8. Number of baffles = 4 mounted vertically at tank wall and extending from the tank bottom to above the liquid surface
 9. Baffle width, $W_b = 1/10$ tank diameter
 10. Central disk diameter, $s = 1/4$ tank diameter

•Metcalf & Eddy, Inc. (2003). *Wastewater Engineering-Treatment and Reuse*, 4th ed., McGraw-Hill, New York, NY.

Turbine - Impeller



Ref: Reynolds, T. D., and P. A. Richards. Unit Operations and Processes in Environmental Engineering. 2nd ed. Boston, MA: PWS Publishing Company, 1996.

Turbine Impeller



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Paddle Mixers

- Paddle mixers consists of series of appropriately spaced paddles mounted on either a horizontal or vertical shaft
- Generally rotate slowly
- Paddles are commonly used as flocculation devices



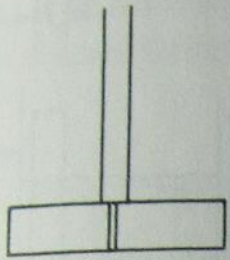
•Ref: http://www.myersequipment.com/jms_gallery_hpwf_12.html

Paddle Mixers

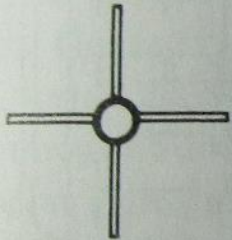
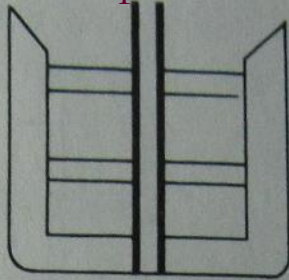
- The diameter of a paddle impeller is usually 50-80% of the tank diameter or width
- Width of a paddle is usually $1/6$ to $1/10$ of the diameter
- Paddles are mounted $1/2$ of a paddle diameter above the tank bottom
- The paddle speeds range from 20 to 150 rpm
- Paddles do not produce turbulence
- Paddle tip speed is generally 0.6 to 0.9 m/s

Paddle Mixers

Four blade paddle



Gate paddle



Ref: Geankoplis C.J. Transport Processes and Separation Process Principles. 4th ed. New Jersey. Prentice Hall. 2003.

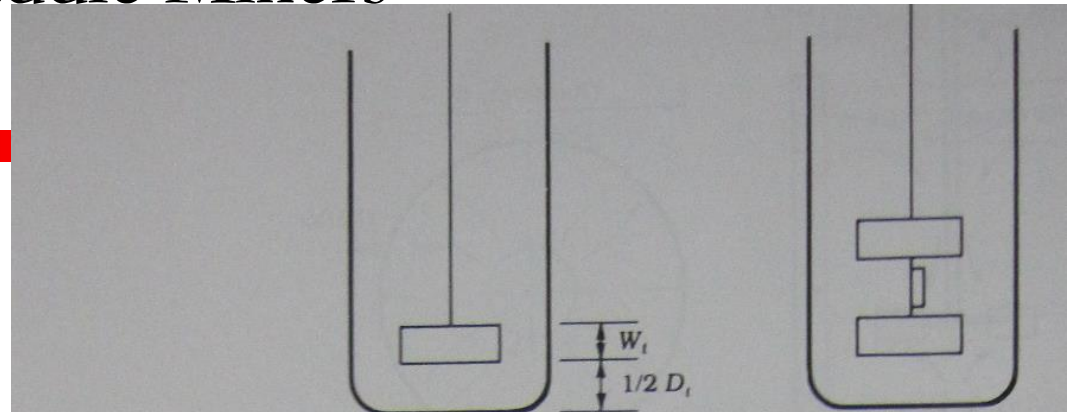


FIGURE 8.12 Types of Paddle Impellers

(a) Two Blades

(b) Six Blades

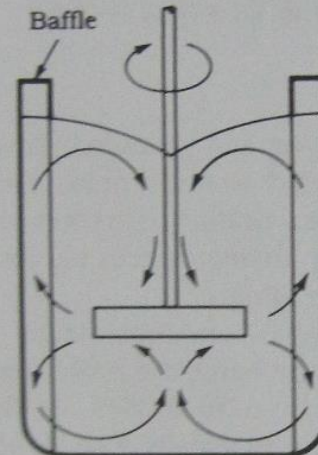


FIGURE 8.13 Flow Regime in a Paddle-

Ref: Reynolds, T. D., and P. A. Richards. Unit Operations and Processes in Environmental Engineering. 2nd ed. Boston, MA: PWS Publishing Company, 1996.

Power imparted to water by a paddle impeller

$$F_D = \frac{C_D A \rho V_p^2}{2}$$

F_D = Drag force (N)

C_D = Coefficient of drag of paddle moving perpendicular to fluid

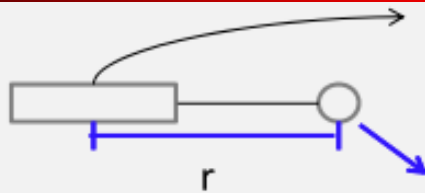
A = Cross sectional area of paddles (m^2)

ρ = density (kg/m^3)

V_p = Relative velocity of paddles with respect to the fluid (m/s), usually assumed to be 0.6 to 0.75 times the paddle tip speed

P = Power requirement (W)

Power imparted to water by a paddle impeller



Shaft (N,rpm)

Velocity of paddle (paddle tip velocity)

$$\frac{2\pi N}{60} r \quad \text{m/sec}$$

1min/60sec

Distance from shaft to paddle center(m)

$$P = F_D V_P = \frac{C_D A \rho V_P^3}{2}$$

Power

Force

Velocity

A=Cross-sectional area of paddle (ft² or m²)
(paddle-blade area at right angle to the direction of movement)

ρ = Density of fluid ($\frac{\text{slug}}{\text{ft}^3}$ or $\frac{\text{kg}}{\text{m}^3}$)

V_P =Relative velocity of paddles with respect to water.

C_d =Drag coeff.

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Power imparted to water by a paddle impeller

THE DRAG COEFFICIENT (C_D) → depends basically on the geometry of the paddle

| L/W ratio | C_D |
|-------------|-------|
| 5 | 1.20 |
| 20 | 1.5 |
| ∞ | 1.90 |

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Pneumatic Mixers

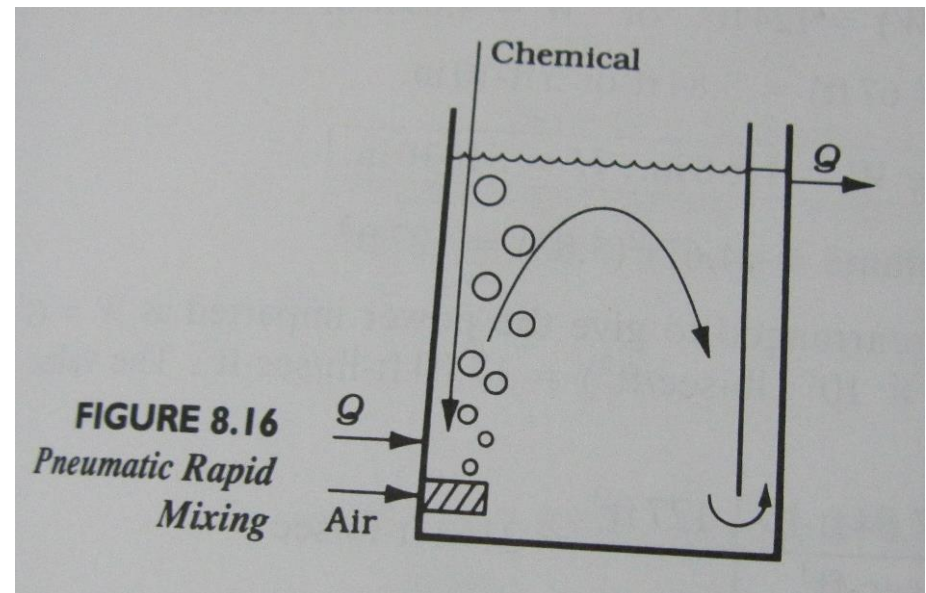
- When air injected in mixing or flocculation tanks or channels, the power dissipated by the rising air bubbles can be estimated by the following equation

$$P = 1.689Q_a \ln \left(\frac{h + 10.33}{10.33} \right)$$

P=Power dissipated (kW)

Q_a =Air flow rate at atmospheric pressure (m^3/min)

h=air pressure at the point of discharge (m)



Ref: Reynolds, T. D., and P. A. Richards. Unit Operations and Processes in Environmental Engineering. 2nd ed. Boston, MA: PWS Publishing Company, 1996.

■ Problems