

MANNING EQUATION APPLIED TO PARTIALLY FILLED CIRCULAR PIPES

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BASIC EQUATIONS

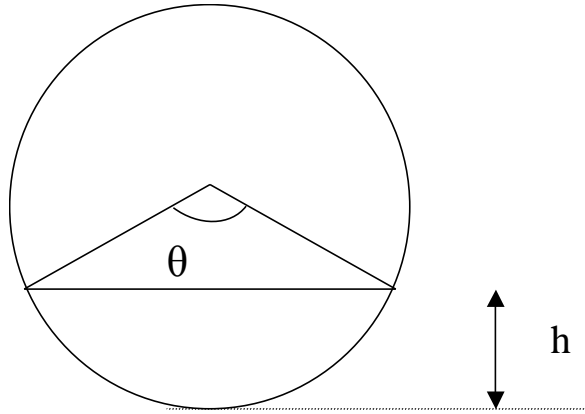
$$V = \frac{1}{n} R_h^{2/3} S^{1/2} \quad (1)$$

$$Q = \frac{A}{n} R_h^{2/3} S^{1/2} \quad (2)$$

$$\theta = 2 \cos^{-1} \left(1 - \frac{2h}{D} \right) \quad (3a)$$

$$A = \frac{D^2}{8} (\theta - \sin \theta) \quad (4)$$

$$R_h = \frac{D}{4} \left(\frac{\theta - \sin \theta}{\theta} \right) \quad (5)$$



Note that the angle θ is expressed in radians. Equation (3a) can be rewritten as follows:

$$\frac{h}{D} = \frac{1}{2} \left(1 - \cos \left(\frac{\theta}{2} \right) \right) \quad (3b)$$

DEFINITION OF K

$$Q = \frac{K}{n} D^{8/3} S^{1/2} \quad (6)$$

$$K = \frac{Qn}{D^{8/3} S^{1/2}} \quad (7)$$

NOTE-1: Metcalf & Eddy (Table 2-5) use the symbol K' for what we denote by K here.

NOTE-2: Metcalf & Eddy use the symbol θ (in Figure 2-25) for half of the surface angle θ .

NOTE-3: In what follows, we will assume the use the metric system (m/sec for V , m for D , and m^3/sec for Q).

TYPES OF PROBLEM THAT REQUIRE ITERATIONS

Iterative calculations are required when h/D is not known in advance. This happens in the following four types of problem:

Type I : Given Q, D, S ; find h/D and V .

Type II : Given Q, D, V ; find h/D and S .

Type III: Given V, D, S ; find h/D and Q .

Type IV: Given Q, V, S ; find h/D and D .

SOLUTION METHODS

TYPE I : Q, D, S are known; find h/D and V

First calculate K using Eq.7. The following three possibilities need considering:

1. If $K > 0.335282$, the problem has no solution.
2. If $0 \leq K < 0.311686$, there is exactly one solution.
3. If $0.311686 \leq K < 0.335282$, there are two solutions, i.e. two possible flow depths.

If $K \leq 0.335282$, you can obtain the “exact” solution(s) by solving the following equation (derived by combining Equations 2, 4, and 5) for θ :

$$K = \frac{2^{-13/3}(\theta - \sin \theta)^{5/3}}{\theta^{2/3}} \quad (8)$$

In case there are two possible θ values, the root found by solving Equation 8 iteratively may depend on the initial guess for θ . To avoid iterations and to ensure that the smaller flow depth is found when there are two possible solutions, use the following approximate explicit equation:

$$\theta = 2 \times 6^{5/13} K^{3/13} \left(1 + 0.431 \sin^{-1}(2.98K) \right) \quad (9)$$

Next, use Eq.3b to calculate h/D . To calculate V , use the following equation:

$$K = \frac{\theta}{2} W^{5/2} \quad (10)$$

The definition of W is given by Equation 18.

EXAMPLE 1 (Problem 6.2.6 in Hwang et al., 2010): A corrugated metal storm water pipe is not flowing full but is discharging $5.83 \text{ m}^3/\text{sec}$. Assuming uniform flow in the 2 m diameter pipe, determine the flow depth if the 100 m long pipe goes through a 2 m drop in elevation.

SOLUTION: In this problem, the following are given: $Q = 5.83 \text{ m}^3/\text{sec}$, $D = 2 \text{ m}$, $S = 2\text{m}/100\text{m} = 0.02$, $n = 0.024$ (from Table 6.2, corrugated metal). Since Q, D , and S are given, this is a Type I problem. Let us calculate K first:

$$K = \frac{Qn}{D^{8/3} S^{1/2}} = (5.83 \times 0.024) / (28/3 \times 0.021/2) = 0.1558$$

Thus, $K < 0.311686$ and there is only one solution. We next estimate this solution:

$$\theta = 2 \times 6^{5/13} \cdot 0.1558^{3/13} \left(1 + 0.431 \sin^{-1}(2.98 \times 0.1558) \right) = 3.13 \text{ radians}$$

Then Eq.3b,

$$\frac{h}{D} = \frac{1}{2} \left(1 - \cos \left(\frac{3.13}{2} \right) \right) = 0.498$$

gives $h/D = 0.498 \approx 0.50$. Therefore, the pipe is 50 % full, and $h = 1 \text{ m}$.

EXAMPLE 2 (Example 2-4 in Metcalf & Eddy, 1981): Determine the depth of flow and velocity in a sewer with a diameter of 300 mm laid on a slope of 0.005 m/m with an n value of 0.015 when discharging $0.01 \text{ m}^3/\text{sec}$.

SOLUTION: Since Q , D , and S are given, this is a Type I problem. Calculate K first:

$$K = \frac{Qn}{D^{8/3}S^{1/2}} = (0.01 \times 0.015) / (0.3^{8/3} \times 0.005^{1/2}) = 0.0526$$

Therefore, $K < 0.311686$ and there is only one solution. An acceptable estimate is:

$$\theta = 2 \times 6^{5/13} 0.0526^{3/13} (1 + 0.431 \sin^{-1}(2.98 \times 0.0526)) = 2.156 \text{ radians}$$

Then

$$\frac{h}{D} = \frac{1}{2} \left(1 - \cos \left(\frac{2.156}{2} \right) \right) = 0.263$$

It is seen that the pipe is 26.3 % full and $h = 79 \text{ mm}$. Velocity is calculated using Eq. 10:

$$V = \left(\frac{2K}{\theta} \right)^{2/5} \frac{D^{2/3} S^{1/2}}{n} = \left(\frac{2 \times 0.0526}{2.156} \right)^{2/5} \frac{0.3^{2/3} 0.005^{1/2}}{0.015} = 0.631 \text{ m/sec.}$$

TYPE II : Given Q , D , V ; find h/D and S

First calculate the quantity $Y = 8A/D^2 = 8(Q/V)/D^2$. You can find the exact value of θ by solving the following equation iteratively:

$$Y = (\theta - \sin \theta) \quad (11)$$

Alternatively, equations developed by Li (1994) can be used:

$$\theta = \frac{Y + \sin \theta_0 - \theta_0 \cos \theta_0}{1 - \cos \theta_0} \quad (0 < Y < \pi) \quad (12)$$

$$\theta = 2\pi - \frac{(2\pi - Y) + \sin \theta'_0 - \theta'_0 \cos \theta'_0}{1 - \cos \theta'_0} \quad (\pi < Y < 2\pi) \quad (13)$$

where $\theta_0 = (6Y)^{1/3}$ and $\theta'_0 = (6(2\pi - Y))^{1/3}$. R_h is next calculated using Equation 5. Next, the slope S can be calculated:

$$S = (nV)^2 R_h^{-4/3} \quad (14)$$

Simpler formulas suitable for quick manual calculations were developed (Akgiray, 2004):

$$\theta = 2.51Y^{-0.34} \left[\cos^{-1}(1 - 0.3183Y) \right]^{1.33} \quad (15)$$

Once θ is computed, Eq. 3b can next be used to calculate h/D . To calculate h/D directly (without calculating θ first), the following approximate relation may be used (Akgiray, 2004):

$$\frac{h}{D} = 0.0047Y^3 - 0.0453Y^2 + 0.2554Y \quad (16)$$

The equation giving the slope is the following:

$$S = \left((D/2Q)^{4/3} V^{10/3} n^2 \right) \theta^{4/3} \quad (17)$$

EXAMPLE 3 (This example was used by Esen (1993) and Li (1994) to illustrate their calculation methods): Calculate the minimum slope of a sewer to carry a flow of $0.01 \text{ m}^3/\text{sec}$. The minimum velocity is specified as 0.5 m/sec and as a preliminary value the diameter of the sewer will be assumed to be 0.45 m . Assume $n = 0.013$.

SOLUTION: Since Q , D , and V are given, this is a Type II problem. Calculate Y first:
 $Y = 8A/D^2 = 8Q/(VD^2) = 8(0.01)/(0.5 \times 0.45^2) = 0.7901$

Although it is not required in this problem, let us first calculate h/D using Eq. 16:

$$\frac{h}{D} = 0.0047(0.7901)^3 - 0.0453(0.7901)^2 + 0.2554(0.7901) = 0.176$$

$$h = (0.45)(0.176) = 0.079 \text{ m} = 79 \text{ mm}$$

Surface angle is estimated as:

$$\theta = 2.51(0.7901)^{-0.34} \left[\cos^{-1}(1 - 0.3183(0.7901)) \right]^{1.33} = 1.7730 \text{ radians}$$

We can now calculate the slope:

$$S = \left((0.45 / 2 \times 0.01)^{4/3} 0.5^{10/3} 0.013^2 \right) 1.773^{4/3} = 0.00229$$

TYPE III: Given V , D , S ; find h/D and Q .

First, calculate the quantity W :

$$W = \frac{Vn}{D^{2/3} S^{1/2}} \tag{18}$$

The following three possibilities exist:

1. If $W > 0.452421$, the problem has no solution.
2. If $0 \leq W < 0.396850$, there is exactly one solution.
3. If $0.396850 \leq W < 0.452421$, there are two solutions, i.e. two possible flow depths.

If $W \leq 0.452421$, you can obtain the “exact” solution(s) by solving the following equation for θ :

$$W = \left(\frac{\theta - \sin \theta}{4\theta} \right)^{2/3} \tag{19}$$

In case there are two possible θ values, the root found by solving Equation 19 iteratively may depend on the initial guess for θ . To avoid iterations and to ensure that the smaller flow depth is found when there are two possible solutions, use the following approximate explicit equation:

$$\theta = 24^{1/2} W^{3/4} \left(1 + 0.255 \left[\sin^{-1}(2.21W) \right]^{2.1} \right) \tag{20}$$

Next, use Eq.3b to calculate h/D and Equation 10 to calculate Q .

EXAMPLE 4 (Example 4-12 in Hammer & Hammer, 1996): An 18-in sewer pipe, $n = 0.013$, is placed on a slope of 0.0025 . At what depth of flow does the velocity of flow equal 2.0 ft/sec ?

SOLUTION: D , S , and V are given. This is a Type III problem. Let us first convert the values of D and V to the corresponding metric units:

$$D = (18\text{in})(2.54\text{cm/in})(1\text{m}/100\text{cm}) = 0.457 \text{ m}$$

$$V = (2.0 \text{ ft/sec})(1\text{m}/3.2808 \text{ ft}) = 0.6096 \text{ m/sec}$$

Next, calculate W :

$$W = \frac{0.6096 \times 0.013}{0.457^{2/3} 0.0025^{1/2}} = 0.267$$

Since $W < 0.39685$, there is exactly one solution. A good estimate is:

$$\theta = 24^{1/2} 0.267^{3/4} \left(1 + 0.255 \left[\sin^{-1} (2.21 \times 0.267) \right]^{2.1} \right) = 2.0 \text{ radians}$$

$$\frac{h}{D} = \frac{1}{2} \left(1 - \cos \left(\frac{2.0}{2} \right) \right) = 0.230$$

Therefore, the pipe is 23 % full, and $h = 0.105 \text{ m} = 4.12 \text{ in}$. Although it is not required in this problem, let us also calculate Q to illustrate the use of Eq. 10:

$$K = \frac{\theta}{2} W^{5/2} = \frac{2}{2} 0.267^{5/2} = 0.037 \Rightarrow$$

$$Q = \frac{K}{n} D^{8/3} S^{1/2} = \frac{0.037}{0.013} 0.457^{8/3} 0.0025^{1/2} = 0.0176 \text{ m}^3 / \text{sec}$$

TYPE IV: Given Q, V, S ; find h/D and D .

First, calculate $A = Q/V$ and then the quantity Z :

$$Z = \frac{Vn}{A^{1/3} S^{1/2}} \tag{21}$$

The following three possibilities exist:

1. If $Z > 0.541926$, the problem has no solution.
2. If $0 \leq Z < 0.430127$, there is exactly one solution.
3. If $0.430127 \leq Z < 0.541926$, there are two solutions, i.e. two possible flow depths.

If $Z \leq 0.541926$, you can obtain the “exact” solution(s) by solving the following equation for θ :

$$Z = \left(\frac{\theta - \sin \theta}{2\theta^2} \right)^{1/3} \tag{22}$$

In case there are two possible θ values, the root found by solving Equation 22 iteratively may depend on the initial guess for θ . To avoid iterations and to ensure that the smaller flow depth is found when there are two possible solutions, use the following approximate explicit equation:

$$\theta = 12Z^3 \left(1 + 0.0765 \left[\sin^{-1} (1.84527Z) \right]^{4.72} \right) \tag{23}$$

Next, use Eq.3b to calculate h/D . To calculate D , use Equation 22:

$$D = \sqrt{\frac{8(Q/V)}{(\theta - \sin \theta)}} \tag{24}$$

EXAMPLE 5: A pipe with a roughness coefficient $n = 0.015$ is to be laid on a slope of 0.004 m/m. The velocity and discharge have been specified as 0.60 m/s and 0.02 m³/s, respectively. Find the necessary pipe diameter and calculate the flow depth.

SOLUTION: This is a Type IV problem. First calculate

$$A = Q/V = 0.02/0.6 = 0.033 \text{ m}^2$$

and then use Equations 21 and 23:

$$Z = Vn/(A^{1/3}S^{1/2}) = 0.442$$

$$\theta = 12(0.442)^3 \left(1 + 0.0765 [\sin^{-1}(1.84527 \times 0.442)]^{4.72} \right) = 1.10 \text{ radians}$$

$$\frac{h}{D} = \frac{1}{2} \left(1 - \cos \left(\frac{1.1}{2} \right) \right) = 0.074$$

Equation 24 is used next to calculate the diameter:

$$D = \sqrt{\frac{8(0.02/0.6)}{(1.1 - \sin 1.1)}} = 1.13 \text{ m.}$$

EXAMPLE 6 (Example 2-5 in Metcalf & Eddy, 1981): Determine the diameter of a sewer required to handle a flow of $0.15 \text{ m}^3/\text{sec}$ when flowing 65 percent full. The sewer is to be laid at a slope of 0.001 m/m and the n value is assumed to be 0.013 .

SOLUTION: In this problem, the following are given: $Q = 0.15 \text{ m}^3/\text{sec}$, $S = 0.001$, $n = 0.013$, $h/D = 0.65$. Since h/D is given, this is not one of the four types of problem that require iterations. Calculations proceed in a straightforward manner:

$$\theta = 2 \cos^{-1}(1 - 2 \times 0.65) = 3.75 \text{ radians}$$

$$A = \frac{D^2}{8} (3.75 - \sin 3.75) = 0.54D^2$$

$$R_h = \frac{D}{4} \left(\frac{3.75 - \sin 3.75}{3.75} \right) = 0.288D$$

$$Q = \frac{A}{n} R_h^{2/3} S^{1/2} = \frac{0.54D^2}{0.013} (0.288D)^{2/3} 0.001^{1/2} = 0.15 \text{ m}^3/\text{sec}$$

From this it follows that $D = 0.604 \text{ m}$.

EXERCISE: Re-work Examples 1 through 5 by solving the applicable equations (Eqs. 8, 11, 19, and 22) by means of manual iterations (i.e. with a hand calculator). Next, solve these equations using software such as the EXCEL Add-in *Solver*. How close are the approximate solutions found here to the “exact” answers you get?

REFERENCES

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